

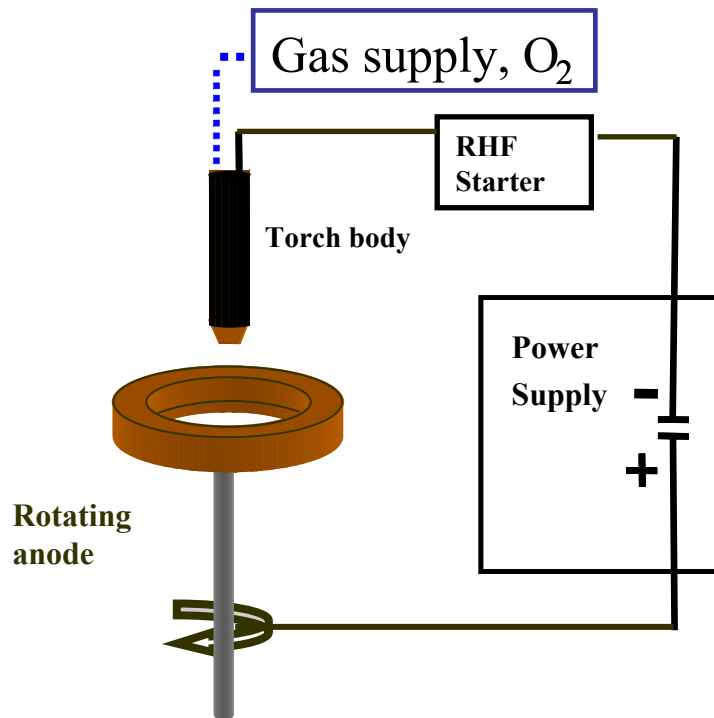
The radial temperature distribution of a constricted oxygen arc in plasma arc cutting

Sung Je Kim

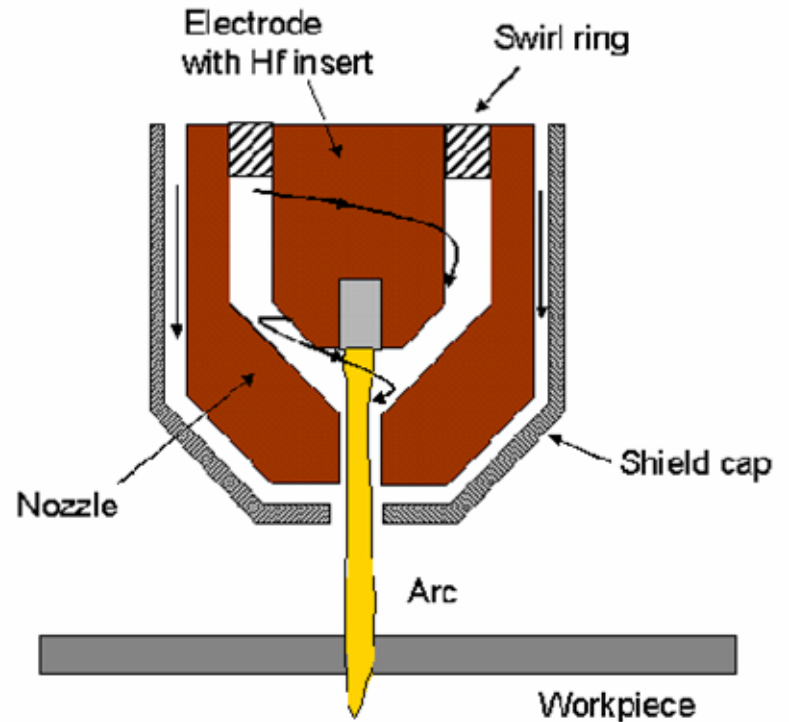
***High Temperature & Plasma Laboratory
University of Minnesota***

Plasma Arc Cutting

Components of cutting system



Cutting torch components



Elenbaas-Heller Equation

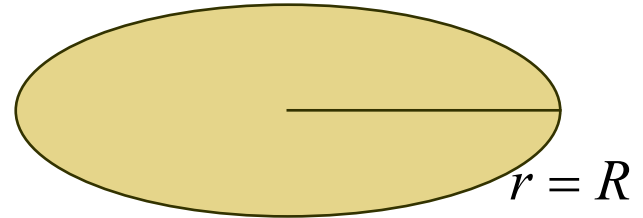
$$\frac{1}{r} \frac{d}{dr} \left[r k(r) \frac{dT}{dr} \right] = \lambda(T) - \sigma(T) E^2$$

$$I = 2\pi \int_0^R E \sigma(r) r dr = 2\pi \cdot E \int_0^R \sigma(r) r dr$$

$$\lambda(T) = 0$$

$$\lambda(T) = 1.18512 \times 10^{10} \left[\frac{T - 4000}{12800} \right]^{4.795} \text{ ergs} / \text{cm}^3 \cdot \text{sec}$$

$$\lambda(T) = 1.8641 \times 10^{16} \text{ ergs} / \text{cm}^3 \cdot \text{sec}$$

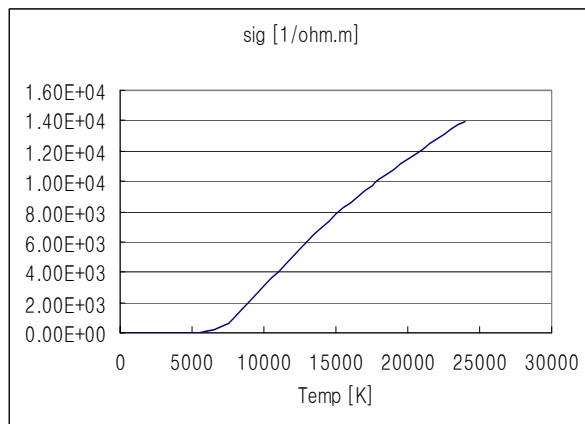


$$0 \leq T \leq 4 \times 10^3 \text{ } ^\circ\text{K}$$

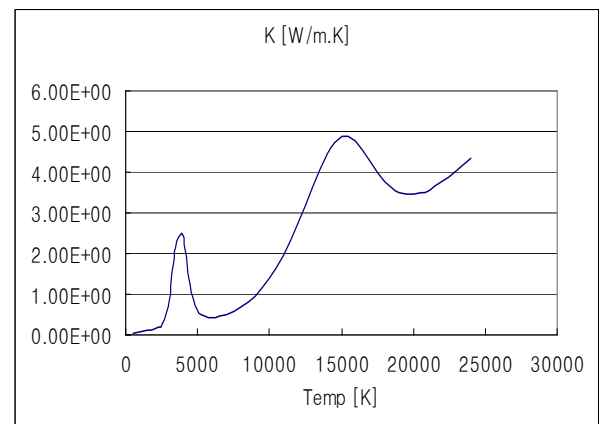
$$4 \times 10^3 \text{ } ^\circ\text{K} \leq T \leq 16 \times 10^3 \text{ } ^\circ\text{K}$$

$$T > 16 \times 10^3 \text{ } ^\circ\text{K}$$

$\sigma(T)$



$k(r)$



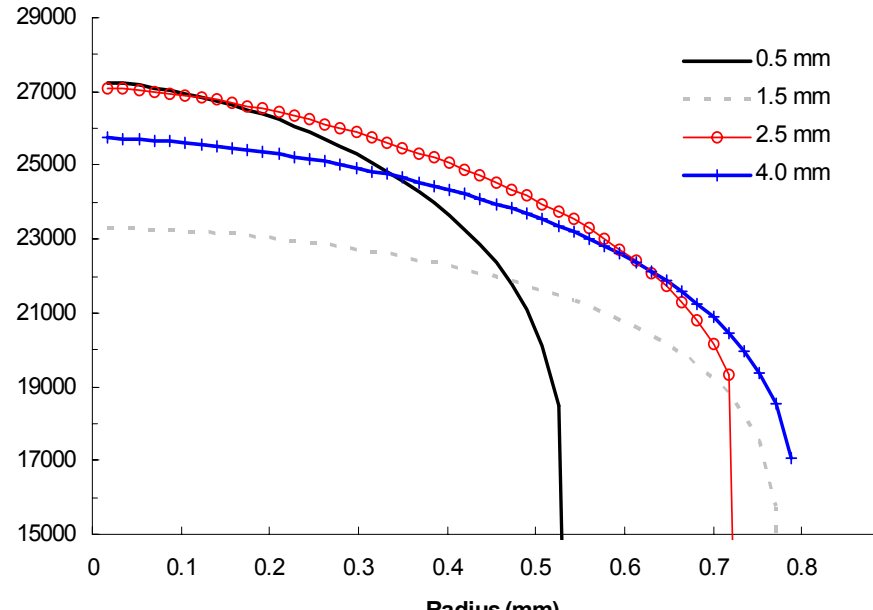
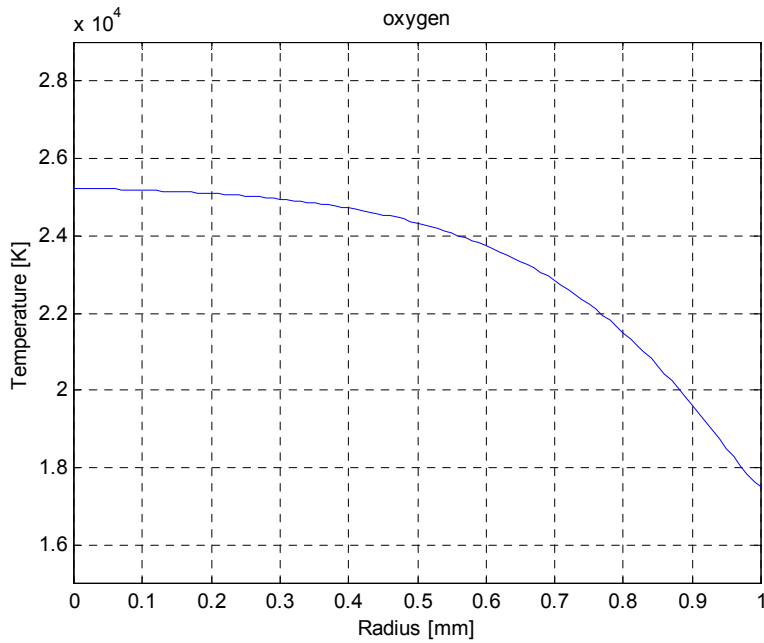
Gauss-Siedel Method



$i=1$ $i=2$ $i=3$

$i=N-2$ $i=N-1$ $i=N$

$$\frac{1}{r_i} \frac{d}{dr} \left(r_{i+1/2} k_{i+1/2} \frac{T_{i+1} - T_i}{dr} - r_{i-1/2} k_{i-1/2} \frac{T_i - T_{i-1}}{dr} \right) = \lambda_i - \sigma_i E_i^2 \quad E_i = \frac{I}{2\pi \sum_i \sigma_i r_i dr}$$



Heat transfer to the anode

$$q_a = j\phi_w + 3.203 \frac{k_B}{e} jT_e - K_h \frac{dT_h}{dx} - K_e \frac{dT_e}{dx} - j_i(\varepsilon_i - \phi_w)$$

$$j = \sigma E_x \quad I = 2\pi \int_0^R jrdr = 2\pi E_x \int_0^R \sigma r dr$$

